## PULSE BROADENING IN MULTIMODE GRADED-INDEX FIBRES

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A closed-form expression is obtained for pulse broadening in graded-index fibres with  $k^2(r) = 1 - r^2 + \epsilon_2 r^4 + \dots + \epsilon_n r^{2n}$ . Pulse broadening for  $k^2(r) = 1 - r^2 + 0 \cdot 615r^4 + 70r^6$  and  $r < 0 \cdot 1$  is 12 times smaller than for square-law fibres if material dispersion is neglected.

When material dispersion can be neglected, the broadening of optical pulses propagating in multimode graded-indexfibres can be evaluated by comparing the optical lengths of rays excited by the source. Recently, Steiner<sup>1</sup> gave a solution based on a vector differential equation for the ray trajectory. The approach proposed in this letter is based on a simpler scalar equation. A closed-form solution is obtained for small, but arbitrary, deviations from a square-law profile.

The Hamilton equations for light rays x(z), y(z) in an isotropic z-invariant medium with wavenumber k(x, y) are

$$dx/dz = k_x/k_z$$

$$dy/dz = k_y/k_z$$

$$dk_x/dz = (1/2k_z)\partial k^2/\partial x$$

$$dk_y/dz = (1/2k_z)\partial k^2/\partial y$$
(1)

The ratio of the time of flight along a ray to the corresponding time along the axis is<sup>2</sup>

$$T = (k_0/k_z)\langle \partial k^2/\partial \omega^2 \rangle/(dk_0^2/d\omega^2) \quad . \quad . \quad . \quad . \quad (2a)$$

where  $k_0 \equiv k(0, 0)$  and  $\langle \ \rangle$  denotes an average over a ray period. When material dispersion can be neglected, eqn. 2a reduces to

The axial component  $k_z$  of k is a constant of motion. From eqns. 1, we obtain

$$\frac{1}{2}k_z^2 d^2(X+Y)/dz^2 = k^2 - k_z^2 + X\partial k^2/\partial X + Y\partial k^2/\partial Y \quad . \tag{3}$$

where  $X \equiv x^2$ ,  $Y \equiv y^2$ . If we integrate eqn. 3 over a ray period, the l.h.s. vanishes because d(X+Y)dz assumes the same value at the limits of integration. Further, if we assume that  $k^2$  is equal to  $k_0^2$  plus a homogeneous function of degree  $\alpha$  in X and Y, we have

In that case, a simple and exact expression for T is obtained:

Our result, eqn. 5, agrees with that given in Reference 3 for the special case

$$k^2 = 1 - (X + Y)^{\alpha} \equiv 1 - R^{\alpha}$$

where  $R \equiv x^2 + y^2 \equiv r^2$ .

Let us now consider a square-law medium ( $\alpha = 1$ )

$$k^2 = 1 - R$$
 . . . . . . . . . . . (6)

The ray equation is easily solved. We obtain

$$R = \frac{1}{2}A(1+\theta) + \frac{1}{2}A(1-\theta)\cos(2z/k_z) . . . . (7)$$

where A denotes the square of the maximum radius of the ray and  $\theta \equiv (L_z/A)^2$ , where  $L_z = xk_y - yk_x$  denotes the axial component of the ray angular momentum (the second constant of motion). For meridional rays, we have  $\theta = 0$ , and, for helical rays,  $\theta = 1$ . For later use, let us evaluate  $\langle R^n \rangle$ . Using the binomial expansion and the result

$$\langle \cos^m \rangle = m! 2^{-m} \{ (m/2)! \}^{-2} \dots \dots \dots (8)$$

for even m,  $\langle \cos^m \rangle = 0$  for odd m, we obtain

$$\langle R^n \rangle = n! 2^{-n} A^n \sum_{m=0, 2}^n \frac{(1+\theta)^{n-m} (1-\theta)^m}{2^m (n-m)! \{(m/2)!\}^2}$$
 (9a)

In particular,

$$\langle R^2 \rangle = A^2 (3\theta^2 + 2\theta + 3)/8$$
  
 $\langle R^3 \rangle = A^3 (1+\theta)(5\theta^2 - 2\theta + 5)/16$  . . . (9b)

Let us now consider a perturbed square-law profile

$$k^2 = 1 - R + \sum_{n=2}^{N} \varepsilon_n R^n$$
 . . . . . . . . (10)

where the  $\varepsilon_n R^{n-1}$  are of order  $\varepsilon$ . For circularly symmetric fibres, eqn. 3 becomes, after integration over a ray period,

$$0 = \langle k^2 - k_z^2 + R \partial k^2 / \partial R \rangle \quad . \quad . \quad . \quad . \quad . \quad . \quad (11)$$

Substituting eqn. 10 in eqn. 11, we obtain, for T in eqn. 2b,

$$T = \frac{1}{2}k_z^{-1}\{k_z^2 + 1 + \sum_{n=2}^{N} (1 - n)\varepsilon_n \langle R^n \rangle\} \quad . \quad . \quad (12)$$

Eqn. 12 is exact. To 1st-order in  $\varepsilon$ , the zeroth-order approximation, eqn. 7, for R can be used in eqn. 12 and  $k_z$  can be expressed in terms of A and  $\theta$ :

$$k_z^2 = 1 - A(1+\theta)$$
 . . . . . . . . . . . (13)

Thus eqns. 9, 13 and 12 give a closed-form expression for the time of flight T of a pulse for any small deviation from a square-law profile.

Let the pulse broadening  $\tau$  be defined as the maximum variation of T for  $0 < \theta < 1$  and  $0 < A < A_0$ . For the square-law fibre in eqn. 6, we obtain  $\tau = 0.5A_0^2 = 20 \times 10^{-7}$  if  $A_0 = 0.002$ . For  $k^2 = 1 - R + \varepsilon_2 R^2$ , we find that T = 1 for meridional rays  $(\theta = 0)$  when  $\varepsilon_2 = 2/3$ , in agreement with

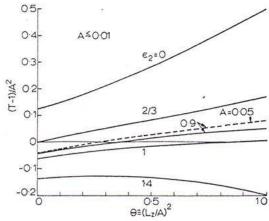


Fig. 1 Variation of pulse broadening in fibre with  $k^2=1-r^2+\varepsilon_2\,r^4$  as function of ray axial angular momentum  $L_z$  for various values of coefficient  $\varepsilon_2$ 

 $\theta = 0$  corresponds to meridional rays and  $\theta = 1$  to helical rays

Reference 4, and T=1 for helical rays  $(\theta=1)$  when  $\varepsilon_2=1$ , in agreement with Reference 5. The variation of T with  $\theta$  for various values of  $\varepsilon$  is illustrated in Fig. 1. The minimum  $\tau$  is obtained when  $\varepsilon_2 = 0.91$ . Then  $\tau = 0.046A_0^2 = 1.84 \times 10^{-7}$ if  $A_0 = 0.002$ . The improvement over the square-law profile is therefore as large as 11. Note that  $\tau/A_0^2$  deviates slightly from a constant if  $A_0$  is not small compared with unity. The broken line in Fig. 1 for  $A_0 = 0.05$  (corresponding to a total variation of refractive index of 2.5%) deviates slightly from the plain line, obtained for  $A_0 \leq 0.01$ . For  $k^2 = 1 - R +$  $\varepsilon_2 R^2 + \varepsilon_3 R^3$ , and  $A_0 = 0.002$ , the minimum  $\tau$  is found for  $\varepsilon_2 = 0.615$  and  $\varepsilon_3 = 70$ : it is equal to  $1.62 \times 10^{-7}$ . The improvement, compared with the case where  $\varepsilon_3 = 0$ , is therefore rather modest. It is interesting, however, that the optimum  $\varepsilon_2$  is so sensitive to the choice of  $\varepsilon_3$ . It is conceivable that the absolute minimum of  $\tau$  would be obtained for a strongly oscillating, ill-behaved, variation of  $k^2$  with r. If this were the case, higher-order terms should be considered before a final conclusion can be reached concerning the optimum profile of a graded-index fibre. The method proposed in this work can also be used to investigate more complicated nearsquare-law fibres, such as the helical fibre 6 with  $k^2 = 1 + 1$  $x^2 - y^2 + \dots$  in a rotating co-ordinate system.

Pulse broadening in square-law and linear-law fibres that have material dispersion is given in Reference 2. More generally, we may have

$$k^{2}(r) = k_{0}^{2} - k_{1}^{2} R + \sum_{n=2}^{N} k_{n}^{2} R^{n}$$
 . . . . . (14)

Proceeding as before, we obtain, for the pulse broadening,

$$T = (k_0/k_z) \left\{ 1 - \frac{1}{2} (1 - k_z^2/k_0^2) D_1 \right\}$$

$$+\sum_{n=2}^{N} \left[ D_n - \frac{1}{2} (n+1) D_1 \right] \varepsilon_n \langle R^n \rangle$$
 (15)

where we have defined the dispersion factors

$$D_n = (k_0^2 dk_n^2/d\omega^2)/(k_n^2 dk_0^2/d\omega^2) \quad . \quad . \quad . \quad (16)$$

that are unity in the absence of dispersion,  $\varepsilon_n \equiv k_n^2/k_0^2$ , and  $\langle R^n \rangle$  is given in eqn. 9 with  $\theta = (L_z/k_1 A)^2$ . Thus a closedform solution for pulse broadening in dispersive fibres that have small, but otherwise arbitrary, deviations from the

square-law has been obtained.

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